

Full-Color Waveguide-type Near-Eye Displays with Huygens' Metasurfaces

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Keywords: metasurface, near-eye displays, holography, waveguide, full color

1 Abstract:

2

3 Miniaturized and lightweight see-through near-eye displays are desirable for wearable
4 computing applications. With the recent rapid advances in ultra-thin metasurface optics, the
5 compactness and weight of near-eye displays can be improved without compromising the
6 performance of the real-virtual scene. In this paper, a proof-of-concept solution, using
7 transparent Huygens' metasurface hologram as the display device, is developed to provide full-
8 color images. A virtual image is created by illuminating three 500 μm metasurface holograms,
9 spaced 500 μm apart, with red, green, and blue light sources, and combining the resulting
10 holographic images in a diffractive waveguide to produce a full-color image in front of the
11 viewer's eyes. Using this method, we experimentally demonstrate a compact and wearable near-
12 eye display with a thin (1.2mm) waveguide in front of the viewer's eyes, creating a virtual image
13 with a large field of view ($\geq 40^\circ$) that can be viewed along with the real world within a large eye
14 box (15mm \times 10mm). To achieve this, we introduce a new design method exploring the
15 potential of metasurface holograms as an image source for mobile computing in daily life.

16

17 1. Introduction

18 Recently, the emergence of the metaverse has sparked a surge of interest in head-mounted
19 displays (HMD) or near-eye displays (NED), which can provide virtual images in front of the
20 viewer's eye. NEDs, which are also treated as the entrance of the metaverse for human beings
21 ^[1-3], can be divided into two types. The first type immerses the user in a completely virtual
22 scene generated by computers, often used in virtual reality (VR) applications ^[4]. To achieve a
23 VR-type NED with a lightweight, large field of view (FOV), large eye box, and high resolution,
24 aspherical plastic optics, Fresnel optics, or holographic optics have been employed to replace
25 traditional spherical glass optics ^[5-6]. A recent emerging approach utilizes catadioptric optics,
26 so-called pancake lenses ^[7-8], to realize an ultra-thin form factor. This is the case, e.g. in the
27 recently released Apple Vision Pro ^[9]. The second type of NED allows the viewers to perceive
28 a mixed-reality world by superimposing virtual information onto real-world scenes, often called
29 optical see-through or augmented reality (AR) NED ^[10-12]. AR NED holds the potential to be
30 essential in our future daily lives, enhancing how we interact with the world and the information
31 around us. For this, typically, partially reflective structures should be employed to achieve the
32 goal of optical see-through, making it more complicated to design an optical see-through NED
33 than an immersive one. To realize them, freeform surfaces and off-axis refractive and reflective

1 structures have been developed ^[13-14]. To obtain a good performance, the optics for these
2 structures should provide a large FOV and exit pupil, which has been proven hard to
3 miniaturize. Among these approaches, the most compact one consists of a projection optics
4 module and a total internal reflection (TIR) waveguide, which can be a geometrical waveguide
5 or a diffractive waveguide ^[15-16]. The light beam from the image source can be collimated with
6 projection optics, then reflected in the waveguide multiple times, and finally coupled out from
7 the waveguide and projected into the viewer's eye. Pupil duplication techniques can be used to
8 enlarge the beam size, and a large eye box is achieved with small exit-pupil projection optics,
9 which can decrease the size of the eyepiece greatly. As for the image source, different types of
10 devices, such as Liquid Crystal on Silicon (LCOS), digital micromirror devices (DMD), organic
11 light emission diodes (OLED), or mini light emission diodes (mini-LED) have been applied ^{[17-}
12 ^{20]}. To make the system more compact, the image source and the projection lens should be
13 optimized together. Despite over seventy years of efforts since the 1960s, balancing and
14 optimizing these performance features of displays simultaneously remains a challenge.

15 Metasurfaces, a new class of ultra-thin planar optical elements consisting of artificially
16 fabricated subwavelength nanostructures, has attracted a lot of interest from both academia and
17 industry, due to its superior modulation capabilities of incident light beam ^[21]. Indeed, these
18 devices offer unparalleled spatial resolution (with pixels that can be sub-wavelength in nature),
19 while enabling almost full and arbitrary control over the local amplitude, phase, and
20 polarization of the wave. Various mechanisms have been adopted to design metasurfaces,
21 particularly those that modulate the phase, ranging from those using resonances, both
22 plasmonic-based ^[22] and dielectric-based ^[23-24], to those using the propagation phase ^[25],
23 geometric phase (Pancharatnam Berry phase ^[26]), or topological phase ^[27]. Thanks to the
24 enormous design degrees of freedom that metasurfaces make accessible, multiple optical
25 functions can be integrated into a single planar device. Also, compared to traditional optical
26 components, metasurface components could miniaturize the system and be fabricated at scale
27 using CMOS-like processes. Due to these attractive properties, various component and system-
28 level demonstrations have been reported, including lensing ^[26, 28-35], holograms ^[36-42], beam
29 bending and steering devices ^[43-48], multifunctional devices ^[49], vortex beam generation ^[50], and
30 many others.

31 As mentioned above, within the context of VR and AR, a lightweight and compact display
32 device with high performance is required. Due to its strong and flexible light-modulating
33 capabilities, metasurfaces can also be introduced in NED to obtain a promising solution to

1 improve performance. A typical NED system consists of an optical magnification subsystem
2 (eyepiece) and an image source. During the usage, virtual images can be generated and loaded
3 on the display device and then imaged at a relatively far distance in front of the viewer's eyes
4 by the eyepiece. The eyepiece is normally a single-component or multi-component lens system
5 or a combination of a projection lens and a waveguide. In this context, metasurface-based
6 components have been exploited to realize or improve some of the functions of the eyepiece in
7 a compact form, e.g. incorporating an element with a large FOV ^[51], reducing the size by
8 employing a full-color achromatic metasurface ^[52-53], integrating a metasurface along with
9 freeform surfaces ^[54], designing a polarization sensitive in-coupler ^[55] or introducing
10 metasurface gratings with high diffraction efficiency ^[56]. Moreover, as a metasurface can
11 provide a virtual image with a large diffraction angle and high diffraction efficiency, it can act,
12 along with an illumination beam, as an image source in NED systems, which can also be
13 explored as an ideal candidate for holographic displays. When a metasurface-based hologram
14 is used as an image source, the display system can be compact and lightweight, with simple
15 reconstruction optics. Indeed, various metasurface holograms have been demonstrated for
16 display applications in recent years ^[36-42]. While most of these demonstrations are static, various
17 material systems (phase change materials, semiconductors, transparent conductive oxides,
18 liquid crystals, etc.) and stimuli (thermal, electrical, and optical) are being explored to realize
19 tunable metasurfaces ^[24] that hold the potential to be used in displays as dynamic SLMs to
20 generate dynamic images or encode computer-generated holograms (CGH). Therefore, the
21 potential ability of metasurfaces, and in particular metasurface holograms, to be used as an
22 image source for different display applications should be explored to provide useful references
23 for the design of future displays. The simplest approach is using a metasurface hologram as an
24 image source for projection-type display, and indeed both single and multiple colors devices of
25 this kind have been demonstrated ^[38-39]. Recently, single-color metasurface holograms have
26 also been used in NED systems as the image source ^[37,57]. For full-color NED systems that can
27 be viewed with the naked eye, however, a holistic design that considers the whole system is
28 crucial, tackling simultaneously many issues that might arise in this type of system, such as
29 color fusion, compactness, image quality, etc.

30 This work demonstrates that three metasurface holograms and small light sources may further
31 miniaturize NED systems with simple optics. As mentioned above, images with three color
32 channels can be projected into waveguides and full-color virtual images can be generated by
33 merging the three channels in the waveguides. Thanks to the high phase mapping resolution of

1 metasurfaces, this type of image source, together with compact lasers, can provide a high-
2 resolution virtual image in a small active display area. Due to the exit pupil expansion feature
3 of diffractive waveguides, a system with a small-size metasurface hologram can achieve an
4 optical see-through image with a large eye box and FOV. Furthermore, virtual images from
5 different projection channels can be merged into a full-color image. Our approach also allows
6 for the metasurface holograms for RGB channels to be designed and fabricated separately,
7 which could be more convenient for bringing dynamic metasurface devices (typically
8 monochromatic) to the future display market. Based on these considerations, we design and
9 experimentally demonstrate a compact full-color waveguide-type NED system using a
10 transmissive dielectric Huygens' metasurface hologram as the image source, able to provide
11 full-color images with a large eye box and a large FOV that can be directly viewed along with
12 the real scene.

13 **2. Results**

14 **2.1. Full-color waveguide-type near-eye displays with metasurface holograms.**

15 As illustrated in **Figure 1**, the display device consists of three metasurface holograms fabricated
16 on a single glass substrate and works with illumination sources (typically three, with three
17 different colors) to project the desired image. Note that each metasurface hologram is
18 wavelength-sensitive and should be designed for the corresponding operation wavelength. An
19 optional color filter can also be used between the illumination sources and the metasurfaces.
20 Since the three small-sized holograms are spatially separated, the virtual images for different
21 color channels may not merge perfectly, resulting in a smaller aperture. In a diffractive
22 waveguide, the beams for different color channels are replicated parallelly by each total internal
23 reflection. Thus, while the images and colors may not overlap perfectly in space, the designed
24 pattern of the waveguide ensures that images for all three colors enter the viewer's eye within
25 the eye box.

26 Additionally, since the diameter of the human pupil is at least 2mm, the aperture of the
27 projection optics should be enlarged to produce a large eye box. The aperture of metasurface
28 holograms is normally in the scale of several hundred micrometer which is much smaller than
29 that of commercial image sources. Thus, the image aperture should be enlarged with the help
30 of the pupil duplication function of the waveguide. Real images far away from the hologram
31 (which can be treated at an infinite distance) can be reconstructed directly by the metasurface

1 when a collimated laser beam illuminates it. Then, after replicating multiple times the beams,
2 they are reflected out of the waveguide and to the viewer's eye by the out-coupler on the
3 waveguide surface with a large eye box. In this design, we can observe the real world through
4 the waveguide, and the holographic image can be superimposed with the real scene.

5 **2.2. Design and performance of the metasurface holograms**

6 Following the design principle described in the previous section, a waveguide-type wearable
7 NED was designed and fabricated. **Figure 2a** shows the system layout. It consists of laser
8 sources, optional color filters, diffractive type waveguides, and metasurface holograms (acting
9 as the image sources). Here, each laser source illuminates the corresponding metasurface
10 holograms, and the holographic images are then projected onto the in-coupler of the waveguide.
11 The axis of laser illumination and the display device is tilted by 25° from the waveguide normal
12 to prevent the possible zeroth order diffraction (direct transmission of incident light) from
13 entering the field of view. The images for the three colors can merge and the eye box can be
14 expanded when they pass through the waveguide. Finally, the full-color image is projected into
15 the viewer's eye via out-couplers, allowing it to be seen along with the real-world scene.

16 Two groups of diffractive elements were designed for the green-blue channel and red channel
17 of the waveguide respectively, due to the wavelength sensitivity of the diffractive structure, and
18 bonded with each other with a protective glass. A three-grating structure was adopted for the
19 waveguide design, consisting of in-coupling grating, turning grating, and out-coupling grating,
20 all embedded into the glass waveguide. The waveguide parameters, layout, and images are
21 shown in **Figures S1-S6** in the supplementary information. The in-coupling grating couples the
22 projection light beam, in which the holographic image information is embedded, into the
23 substrate, which then guides it towards the turning grating, which directs light toward the
24 outcoupling grating. The pupil is duplicated and enlarged vertically by the turning grating and
25 is expanded horizontally by the outcoupling grating before the light beam reaches the viewer's
26 eye. The parameter selection of these gratings for different wavelengths has been discussed in
27 previous works ^[57-58] and is schematically shown in **Figure S2**. In the diffractive waveguide,
28 the beams for different color channels are replicated parallelly at each reflection. To obtain a
29 large eye box and an image with full color, the design parameters, including the refractive index,
30 thickness, and phase distribution of each grating, were analyzed and optimized using
31 commercial optical design software (Synopsys Lighttools), as shown in **Figure S7**. As the eye
32 pupil cannot be less than 2mm, the distance between adjunct beams emitting from the

1 waveguide should not be larger than 2mm. Based on the optimized parameters, images
2 projected from each metasurface holograms with an aperture of 0.5mm can be viewed by the
3 viewer's eye within an eye box of 15mm × 10mm and with a field of view of 40 degrees. **Figure**
4 **S8** also gives the diffraction efficiency of the waveguide as a function of wavelength, which
5 can reach the average level of commercial products.

6 For the color image demonstration, three 500μm × 500μm metasurface holograms based on
7 TiO₂ nanoantennas are used as the red, green, and blue (RGB) channels of the virtual images.
8 To achieve the full 0-2π phase control in transmission with reduced fabrication aspect ratios,
9 we choose to use Huygens'-type metasurfaces. They enable high transmission and 2π phase
10 modulation simultaneously by carefully tuning the spectral positions of the electric dipole (ED)
11 and magnetic dipole (MD) resonances excited in the nanoantennas. When the induced dipole
12 moments associated with ED and MD have the same amplitude and phase, the backward
13 scattering from the nanoantennas is suppressed, which means the Huygens condition is met.
14 This results in a near-unity transmission through the metasurface with a 2π phase modulation
15 around the resonant wavelength [45, 60, 61]. For our operation wavelengths of 662nm (red, R),
16 532nm (green, G), and 473nm (blue, B) the following nanoantenna heights and lattice pitches
17 have been selected through design optimization: h_R = 172nm and P_R = 420nm for red, h_G =
18 125nm and P_G = 340nm for green, and h_B = 113nm and P_B = 305nm for blue. The simulated
19 performance of the designed, disk-shaped TiO₂ Huygens metasurfaces is presented in **Figure**
20 **2**. The nanodisks are arranged in a square lattice and placed on a SiO₂ substrate. For each
21 specific wavelength, the thickness and diameters of the disks are optimized using a commercial
22 finite-difference time-domain (FDTD) simulation software (ANSYS Lumerical) to achieve the
23 Huygens condition at the corresponding wavelength, and a periodical boundary condition is
24 used for the simulation. The parameters to accomplish the Huygens' condition are summarized
25 in Table S1, and the transmission and phase modulation spectra of the nanoantenna designed
26 for RGB channels are shown in **Figure 2c-e**. From the transmission spectrum, we can see the
27 merge of the corresponding ED and MD dips in the spectrum, and the transmission is larger
28 than 0.9 for green and blue, and 0.85 for red, at the same time there is a 2π phase shift around
29 that operational wavelengths. This is a typical feature of the Huygens metasurface[45]. The
30 electric and magnetic field distribution in the antenna designed for wavelength 532nm at
31 Huygens condition is shown in supplementary materials. After obtaining the optimized
32 diameter of the nanodisk, they are varied around the optimized value, as shown in **Figure 2f-h**,
33 to induce the phase modulation of ~2π. Over the 2π range, 8 phase levels corresponding to the

1 phase modulations step of $\pi/4$ are chosen to digitalize the holograms. With the change in the
2 diameter of the nanodisk, the transmission drops due to the partial detuning of the overlap of
3 the ED and MD dipole. It is slightly off the exact Huygens condition. It is worth noting that the
4 phase modulation for each wavelength falls in a limited spectrum range, as shown in **Figure 2i**,
5 and there is a clear separation between red, green, and blue colors. To check the performance
6 of the designed metasurface, nanodisks with different diameters corresponding to the 8 equally-
7 spaced phase levels covering the 2π phase range were arranged in a supercell to form a blazed
8 phase grating. The diffraction efficiencies of these blazed gratings for different colors were
9 numerically calculated and summarized in Table S2 and shown in **Figure 2j**.

10 To compute the point-cloud-based phase-type holograms a coherent ray tracing approach ^[62]
11 was used. The coherent ray tracing algorithm is selected in this report, as it can provide high-
12 quality reconstruction and can support large-angle displays. As mentioned above, the projection
13 plane of the generated holographic image can be infinitely far away. Here a large distance of
14 around 10cm is used, which, compared to the $500\mu\text{m} \times 500\mu\text{m}$ hologram size, can be treated
15 as infinite. A point cloud image comprising three sets of letters "A*STAR", "BIT" and "NTU"
16 surround a symbol of a star, and two flower symbols are selected to verify the proposed display
17 method, which contains both separate colors and merged color image parts (**Figure 2b**). Each
18 generated point can be treated as a point-light source and is propagated to the hologram plane.
19 The complex field distributions at the hologram plane from point sources are summed up and
20 form a complex hologram, in which all the information about the object is encoded. Due to the
21 complexity of independently manipulating amplitude and phase, the amplitude information in
22 the complex hologram is discarded and the amplitude is set to unity, thus forming a pure phase-
23 type hologram. Finally, the obtained phase profile is mapped with the designed nanoantennas
24 forming the final metasurface hologram.

25 To achieve the different required heights the three metasurface holograms (R, G and B) were
26 fabricated on one glass plate with a relatively large separation distance of 0.5mm via a specially
27 developed staircase lithography process (see more details in Methods). In brief, the three
28 metaholograms are first patterned and transferred into a 180nm thick TiO₂ film using electron
29 beam lithography and etching. The red metahologram is then masked with a protective layer,
30 and the metaholograms patterns for green and blue channels are further etched down to the
31 desired thicknesses using an ICP dry etching process. Then, the protective layer for the red
32 metahologram is removed by heating the sample in a Piranha bath. A characteristic scanning
33 electron microscope (SEM) image of one of the holograms is shown in **Figure S10**. Before

1 assembling the fabricated holograms as image sources for the NED, their peak diffraction
2 efficiencies are measured to be 8.01%, 14.05%, and 15.75% at wavelengths of 658nm, 510nm,
3 and 468nm, respectively (**Figure 2k**). Compared to the simulated diffraction efficiencies
4 (30.2%, 36.0%, and 32.5% for red, green, and blue) shown in **Figure 2j** for 8-phase level blazed
5 gratings, the peak positions matched well with the designed wavelengths for red (662nm) and
6 blue (473nm) channels. A slightly larger deviation is observed for the green channel (510nm vs
7 532nm), which can be attributed to fabrication imperfections. The moderate diffraction
8 efficiencies of the Huygens' metaholograms can be explained by inter-particle coupling in the
9 arrays, which causes a deviation of the experimental phase values from the simulated ones
10 (since the simulations are done for the uniform nanoantenna arrays and the measurements are
11 for the non-uniform hologram patterns).

12 **2.3 Performance of the near-eye displays using the metasurface holograms**

13 A prototype of a waveguide-type near-eye display was set up with the fabricated metasurface
14 holograms based on the design described in the previous sections. **Figure S11** shows a photo
15 of the assembled setup. A white screen was used to display the projection image, and a single-
16 lens reflex camera was used to capture the image. **Figure 3** shows the projection performance
17 of the metasurface hologram, including the results of any two of the R, G, and B channels.
18 Images with full color can be seen on the screen, e. g. white color can be obtained by merging
19 all three channels. It should be noted that the merged image has a slight displacement due to
20 the separate design structure for the three holograms. Off-axis illumination methods, as
21 demonstrated in previous studies ^[63-64] can be used, which can reduce the crosstalk and
22 displacement among different wavelengths by obliquely projecting laser beams onto the
23 metasurface. In our proposed near-eye display method, the illumination method can be achieved
24 by an easy way, and the displacement can be solved within the waveguide due to the pupil
25 duplication properties.

26 To make the system easy to wear, a spectacle frame is designed and manufactured by 3D
27 printing to hold the laser source, the waveguide, the mirrors, the metasurface holograms, and
28 the optical attenuator (optional), which is shown in **Figure S12**. Here, a button cell or other
29 portable power devices can be used to power the laser source, and an optical attenuator is
30 included to reduce the intensity of the light to protect the eyes. In the future, when dynamically
31 tunable metasurface devices are developed, a compact full-color AR near-eye display with a
32 better design can be achieved using the proposed method. **Figure 4** shows the augmented

1 information displayed by the system and the real world, as captured by the single-lens reflex
2 camera. As can be seen, the reconstruction through the waveguide system is not as good as the
3 hologram reconstruction in the free space shown before. This is mainly due to the stray light
4 within the waveguide and the speckle noise caused by using a laser as the illumination source.
5 The stray light can be further reduced by optimizing the structure of the waveguide, and the
6 speckle noise can be removed using different approaches such as random phase averaging
7 and/or camera-in-the-loop neural network algorithms ^[11]. All these techniques and the
8 possibility of using dynamically tunable metasurface devices can be introduced to improve
9 image quality in the future. We note that the transmissive character of the metasurfaces or their
10 physical separation is not an essential feature and slightly modified designs could be adapted
11 for reflective metadevices or time-sequential color rendering.

12 **3. Conclusion**

13 In summary, we have proposed and demonstrated a proof-of-concept solution for a full-color,
14 lightweight, and compact NED system including three separated transmissive metasurface
15 holograms as the image sources. These spatially separated metaholograms can be fabricated on
16 the same substrate with a so-called staircase metasurface fabrication method. A diffractive
17 waveguide is then utilized to enlarge the projection aperture of the metasurface holograms and
18 merge them into a full-color virtual image that can be observed directly by the viewer's eye
19 within a large eye box. The developed method can ultimately miniaturize the current NED
20 systems, promoting the development of mobile AR on smartphones and wearable AR products
21 displays in the consumer electronics market in the future, finding widespread applications in
22 our daily lives.

23 **4. Methods**

24 **Metasurface Hologram Fabrication Process:** Figure S13 shows the fabrication process of
25 metasurface hologram. First, titanium dioxide (TiO₂) film of 180 nm in thickness is deposited
26 using a dual beam ion-assisted deposition system (Oxford Optofab 3000) on a 2.5 cm × 2.5 cm
27 quartz substrate with 0.7 mm thickness. The complex refractive index of TiO₂ is measured using
28 spectroscopic ellipsometry (Woollam) and is used to determine the precise film thickness using
29 the Filmetrics tool. After that, a 30 nm Cr thin film is evaporated on top of the TiO₂ layer using
30 an electron beam evaporator (Angstrom), followed by spin coating and soft baking of negative
31 tone electron beam resist Hydrogen Silsesquioxane (HSQ). Three arrays of 500 μm × 500 μm

1 dimensions (corresponding to red, green, and blue color hologram channels) separated by 500
2 μm gaps are patterned using electron beam lithography (Elionix ELS-7000), followed by the
3 development of patterns in a salty developer (NaOH/ NaCl). The HSQ patterns are used as
4 masks to etch the chromium (Cr) layer underneath using an Oxford Plasma Etch, which is an
5 inductively coupled plasma (ICP) reactive ion etching (RIE) tool, using Cl_2 and O_2 gases. The
6 etched Cr disk patterns are then used as masks to etch the underlying TiO_2 using CHF_3 gas in
7 the SPTS (KLA) tool (ICP RIE). Cr patterns are then removed using wet chemical etching using
8 commercial Cr etchant. All three metasurface arrays now consist of nanodisks with 180 nm
9 thickness. To reduce the thickness of TiO_2 nano disks corresponding to G and B metasurfaces,
10 the R metasurface is masked by spin coating the substrate with positive S1811 photoresist
11 (thickness $\sim 1.5 \mu\text{m}$), followed by exposing the resist in a mask aligner (EVG 62008 Infinity)
12 with 405nm light through a photomask which blocks the R metasurface array with a square of
13 $525 \mu\text{m} \times 525 \mu\text{m}$ and let the rest of the resist expose. After developing the pattern, the substrate
14 is put through another ICP RIE process to reduce the height of G and B arrays, while the R
15 array stays unaltered under the resist mask. After the height reduction, the resist mask from R
16 is removed by heating the substrate in a Piranha solution bath.

17 **Diffraction Waveguide Fabrication Process:** The full-color waveguide consists of one
18 protective glass (SCHOTT BK7) and two pieces of diffractive waveguides with different
19 parameters. Both waveguides are made of glass (Hoya TAFD25, refractive index of 1.9) with
20 a thickness of 0.35 mm. The gratings are made from a photoresist (Inkron IOC-133, refractive
21 index of 1.9) using nanoimprinting (Obducat Eitre TM 8 NanoImprinter). The imprint mold for
22 the nanoimprinting process is fabricated by Electron Beam Lithography (JEOL JBX-9500FS)
23 with dry-etching technology (Lam Research 2300 kiyo 45). **Figure S14** shows the fabrication
24 process of the nanoimprint mold. A UV gel is used to integrate the waveguide and an air gap
25 of 0.1mm is set between the waveguides, which guarantees the total internal reflection.

26 **Characterization and measurements:** The size and morphology of the metasurfaces are
27 characterized by a scanning electron microscope (Hitachi SU8220). To measure the diffractive
28 efficiency of the metasurface hologram, a supercontinuum source (SuperK EXTREME, NKT
29 Photonics) along with a tunable filter (SuperK SELECT, NKT Photonics) is used as the light
30 source. The intensities of the incident light and the generated images are measured with an
31 optical power meter (Thorlabs PM320E Model Console + S120C Detector). The display
32 performance is recorded by a single-lens reflex camera (SONY $\alpha 7$ IV, with a standard lens of
33 FE35mm F1.8). To meet the Huygens' metasurface operation requirements, the laser beam is

1 collimated and incident normally to the metasurfaces. The beam size is controlled with a
2 pinhole (diameter of $500\mu\text{m}$) to cover the hologram ($500\mu\text{m} \times 500\mu\text{m}$) appropriately. The
3 incident light intensity is measured after the pinhole and before the hologram. The intensity of
4 the reconstructed image is measured with the help of a condenser lens to guarantee the diffracted
5 light is correctly collected by the photodetector of the power meter. The diffraction efficiency
6 is calculated as the ratio of the first-order diffraction intensity to the incident light intensity.

7 **Acknowledgments**

8
9 **Funding:** This work was supported by the National Natural Science Foundation of China
10 (62475013,62332003), A*STAR RIE2020 AME Programmatic Funding (A18A7b0058), and
11 the National Research Foundation of Singapore under Grant No. NRF-NRFI2017-01.

12 **Conflict of interest:** The authors declare no conflict of interest.

13 **Author Contributions:** W.S. and X.L. contributed equally to this work. W.S., X.L., Q.C, Y.Z.,
14 R.P.D, and A.I.K. conceived the idea and designed the experiments. W.S, X.L, X. S. and Y.W
15 designed the optical system, calculated the hologram, and characterized the display
16 performance. X.X and P.M. performed the design, optimization, fabrication, and
17 characterization of the metasurface. W.S., X.L., Q.C., Y.Z., R.P.D., and A.I.K. co-wrote the
18 paper. All authors contributed to the analysis and discussions of the results.

19 **Data and materials availability:** All data needed to evaluate the conclusions in the paper are
20 present in the paper and/or the Supplementary Materials. Additional data related to this paper
21 may be requested from the authors.

22

23 Received: ((will be filled in by the editorial staff))

24 Revised: ((will be filled in by the editorial staff))

25 Published online: ((will be filled in by the editorial staff))

26

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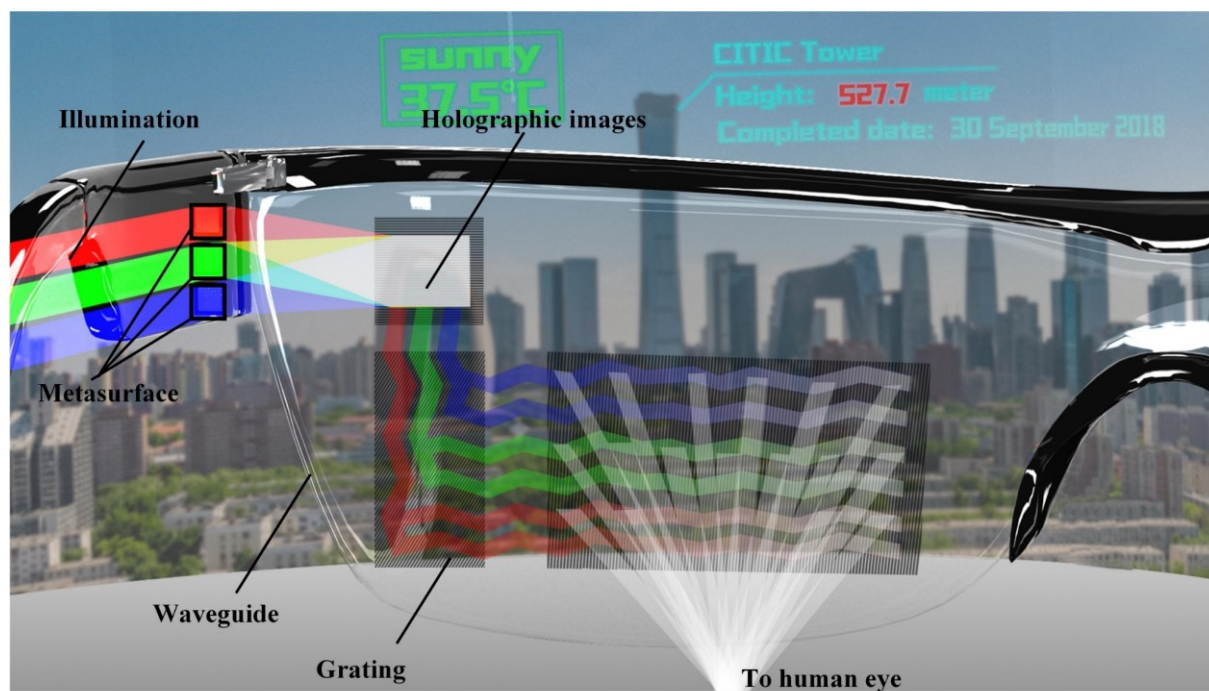
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1 **Figures and Captions**

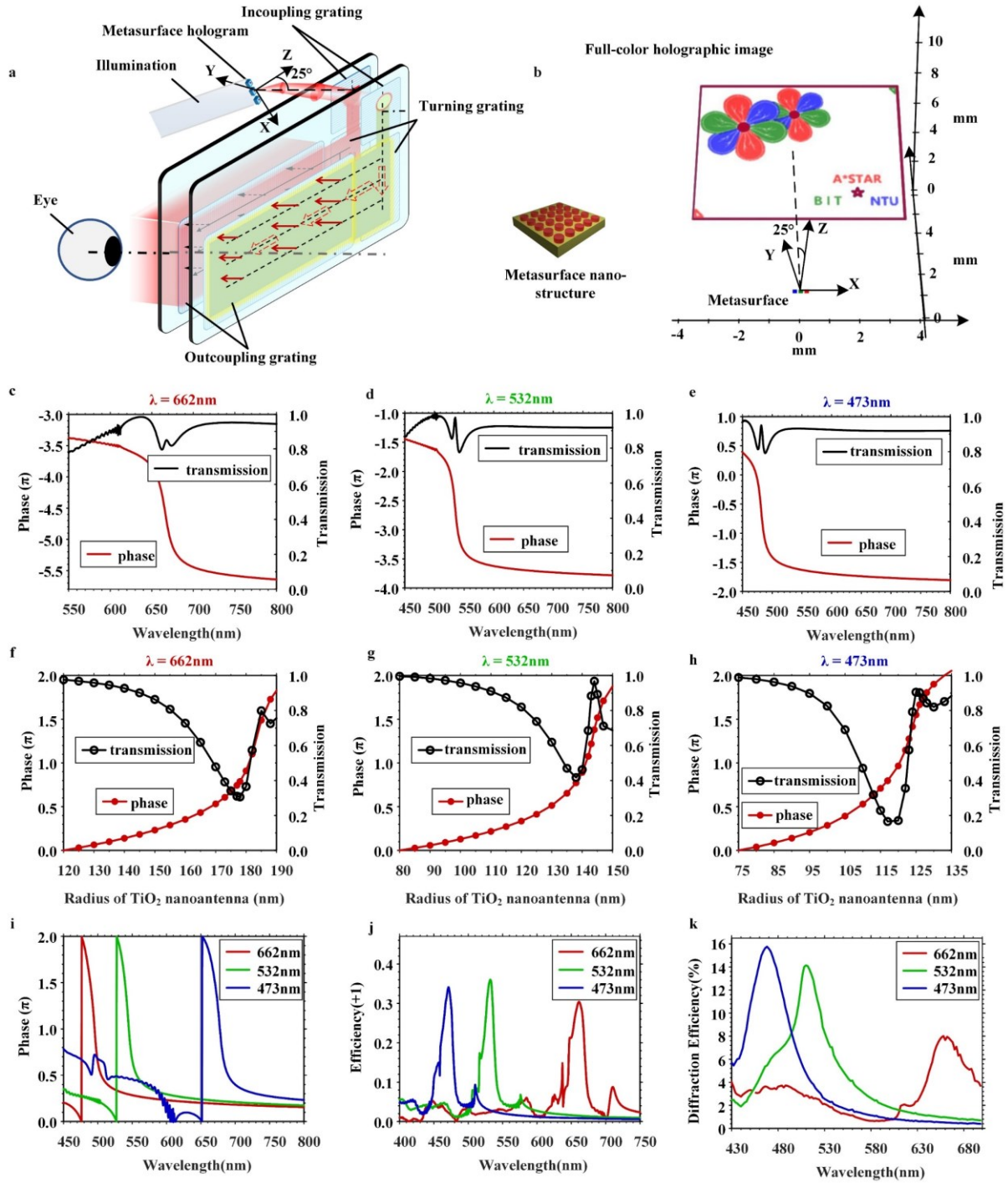
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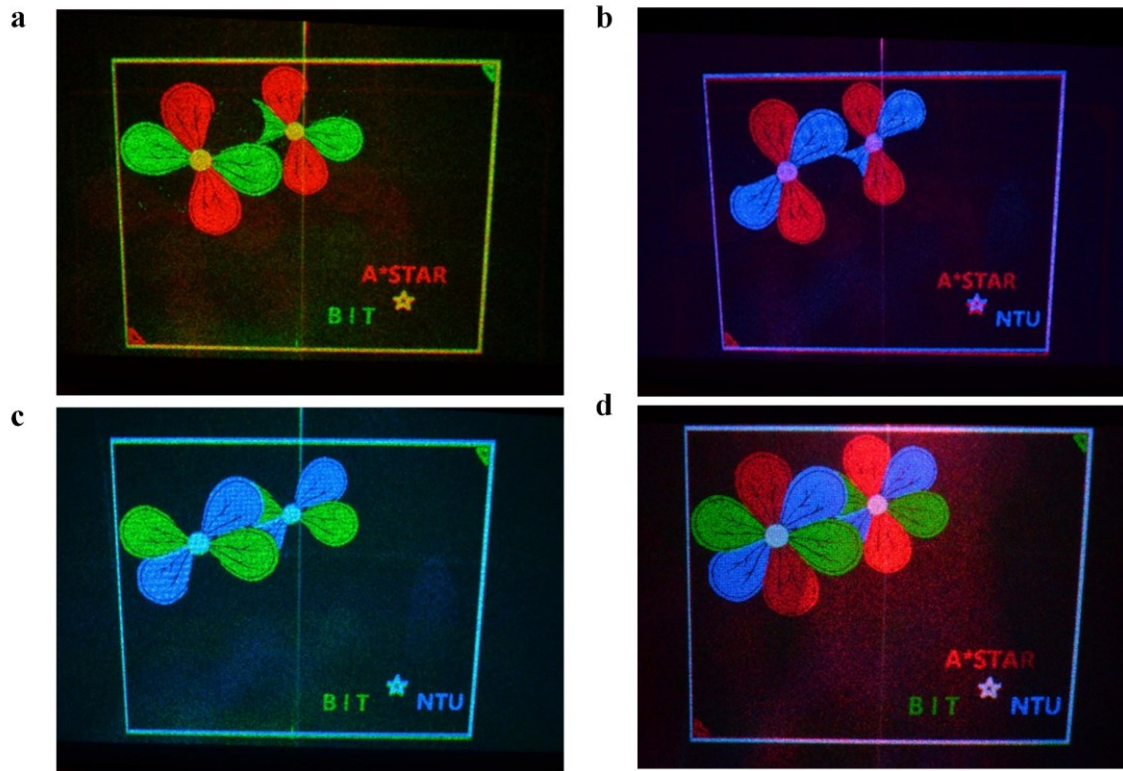
4 **Figure. 1. General illustration of a full-color waveguide-type near-eye display with**
5 **Huygens' metasurfaces.**

6



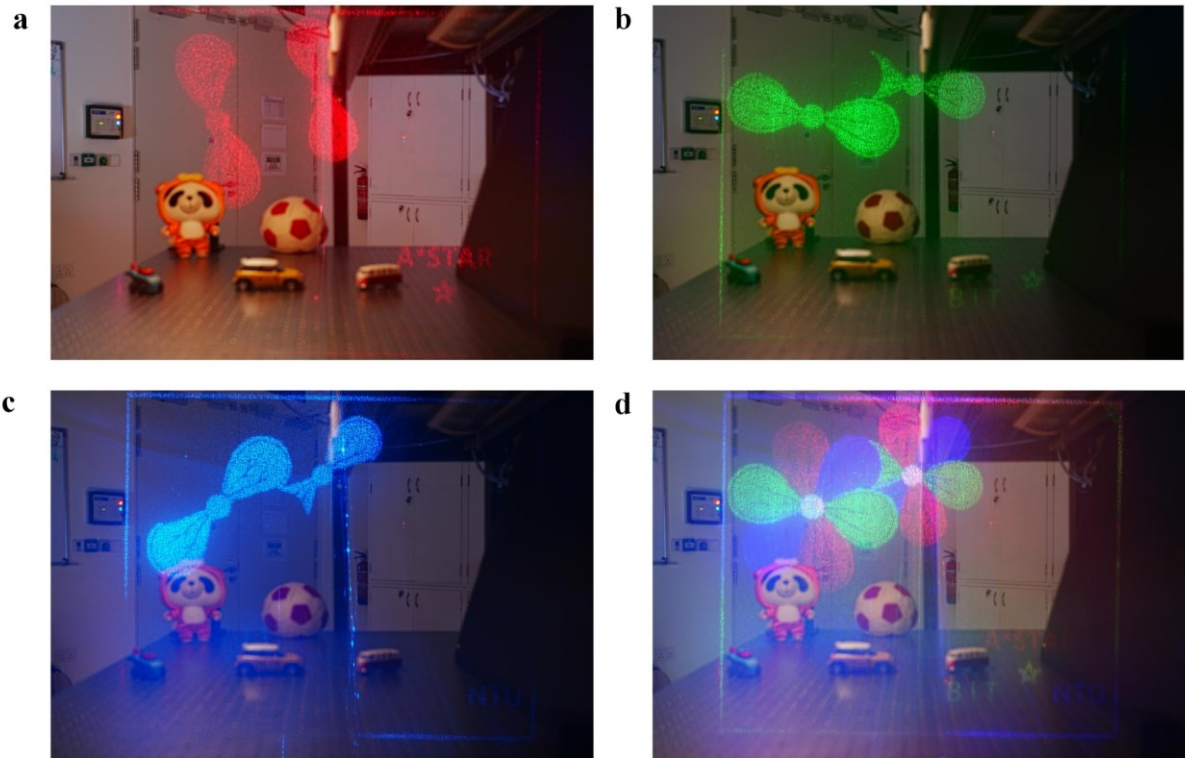
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 2 **Figure 2. System schematic and design of the metasurface hologram.** (a) Illustration of the
 3 setup of an optical see-through full-color near-eye display system using transmissive
 4 metasurface holograms. (b) Spatial position of the reconstructed color images with respect to
 5 the metasurface holograms. (c-e) Simulated transmission spectra and phase modulation for
 6 uniform TiO₂ nanoantenna arrays optimized to achieve Huygens' Condition at R, G, and B
 7 wavelengths respectively (see the array parameters in Table S1). (f-h). Simulated 0 ~ 2π phase
 8 modulation together with the transmission spectra from uniform TiO₂ nanoantenna arrays with
 9 varied nanoantenna radius around the Huygens' condition at (f) R, (g) G, and (h) B wavelengths.

- 1 **(i)** phase modulation at RGB wavelengths **(j)** Simulated beam deflection efficiency by 8-phase
- 2 level blazed metasurface grating at RGB wavelengths. **(k)** Measured diffraction efficiencies for
- 3 the generated images from RGB holograms as a function of the wavelength (normalized to the
- 4 incident light)
- 5



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Figure 3. Projection images using the designed metasurface holograms for two channels of (a) red & green, (b) red & blue, and (c) green & blue, and (d) all three red, green & blue channels together, are projected on the white screen and captured by the single lens reflex camera.



1
2 **Figure 4. Optical see-through near-eye display using the designed metasurface holograms.**
3 **(a-c)** generated images for a single channel of **(a)** red, **(b)** green, and **(c)** blue, captured by a
4 single-lens reflex camera along with the real-world scene. **(d)** Augmented full-color
5 information is displayed by the system along with the real-world scene.

6

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2 **Supporting Information**

3

4 **Full-color Waveguide-type Near-Eye Displays with Huygens' Metasurfaces**

5

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5 **Supporting Information**

6 Figure S1. Illustration of grating patterns on the waveguides (units, mm).

7 Figure S2. Illustration of diffraction structures nano-printed on waveguide surfaces (units, nm).

8 Figure S3. Top-view (left) and cross-sectional (right) SEM images of the in-coupling grating
9 for the green-blue channel waveguide.

10 Figure S4. Cross-sectional (left) and top-view (right) SEM images of the turning grating for the
11 green-blue channel waveguide.

12 Figure S5. Cross-sectional (left) and top-view (right) SEM images of the outcoupling grating
13 for the green-blue channel waveguide.

14 Figure S6. Photographs of (a) imprint mold and (b) uncut waveguide, showing two steps of the
15 waveguide fabrication process.

16 Figure S7. Simulation results of beam distribution within the eye box for different fields of
17 angles.

18 Figure S8. Diffraction efficiency of the waveguide as a function of wavelength.

19 Figure S9. The electric field profile (left) and magnetic field profile (right) in the nanodisk
20 designed for the wavelength of 532nm at Huygens condition.

21 Figure S10. SEM image of a metasurface hologram fabricated with the staircase fabrication
22 process.

23 Figure S11. System set-up for image projection using the designed metasurface holograms.

24 Figure S12. Possible near-eye display system set-up using the designed metasurface holograms.

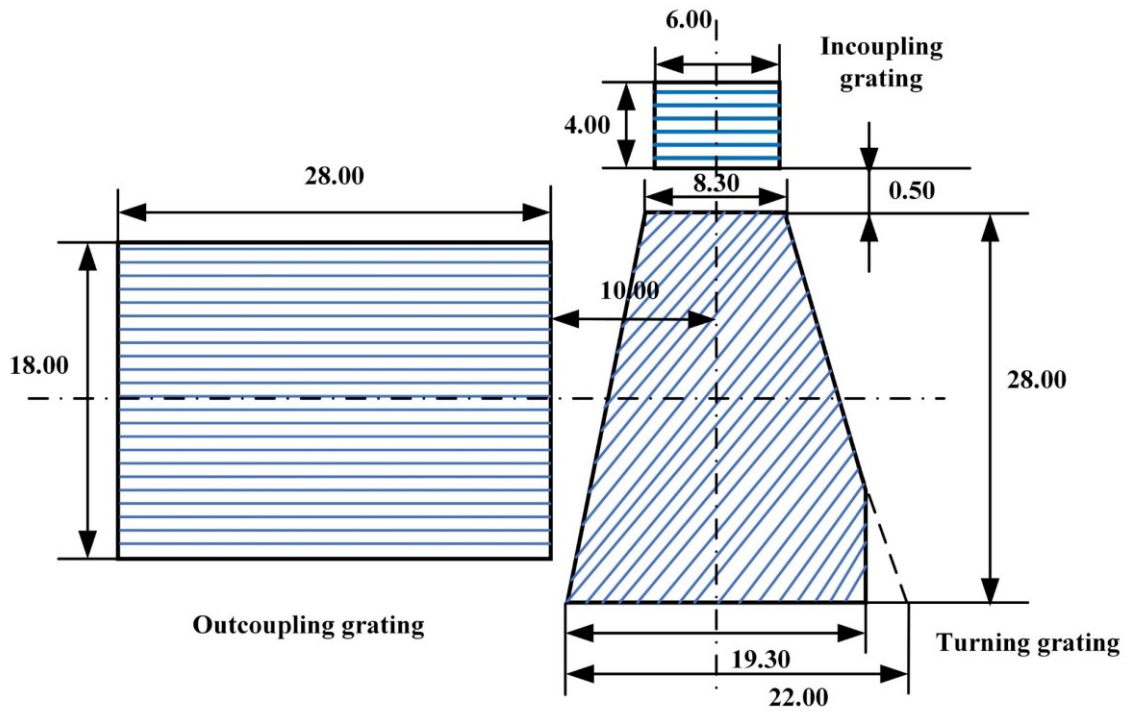
25 Figure S13. Fabrication process of metasurface hologram.

26 Figure S14. Fabrication process of nanoimprint mold.

27 Table S1. Design parameters of TiO₂-based transmissive Huygens' metasurfaces.

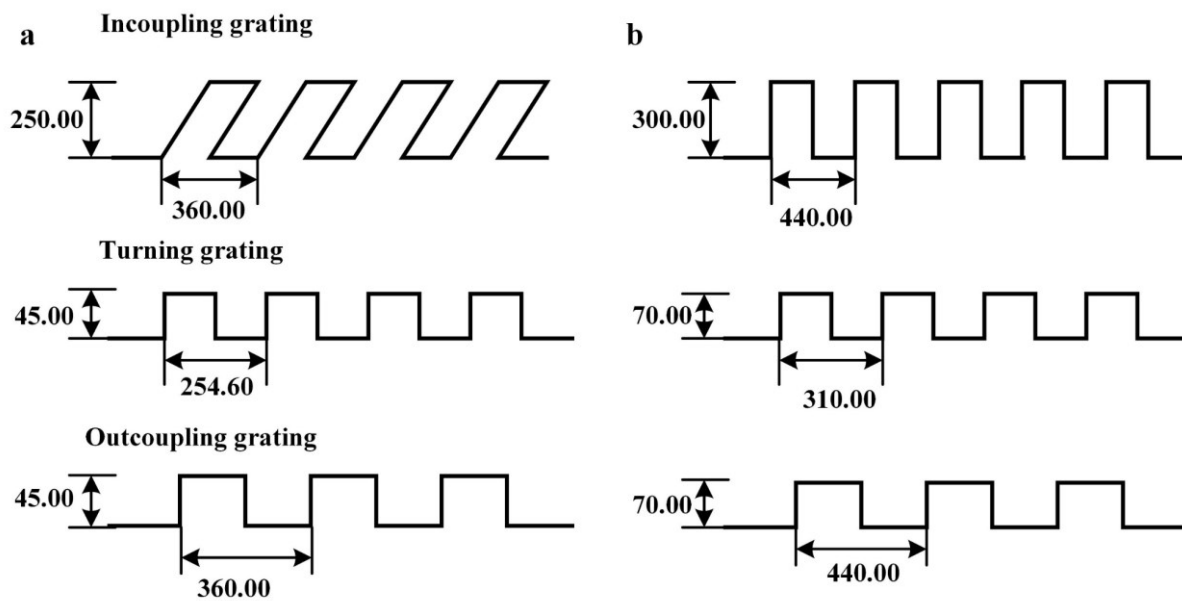
28 Table S2. Simulated beam deflection efficiency at RGB wavelengths for the blazed gratings.

29



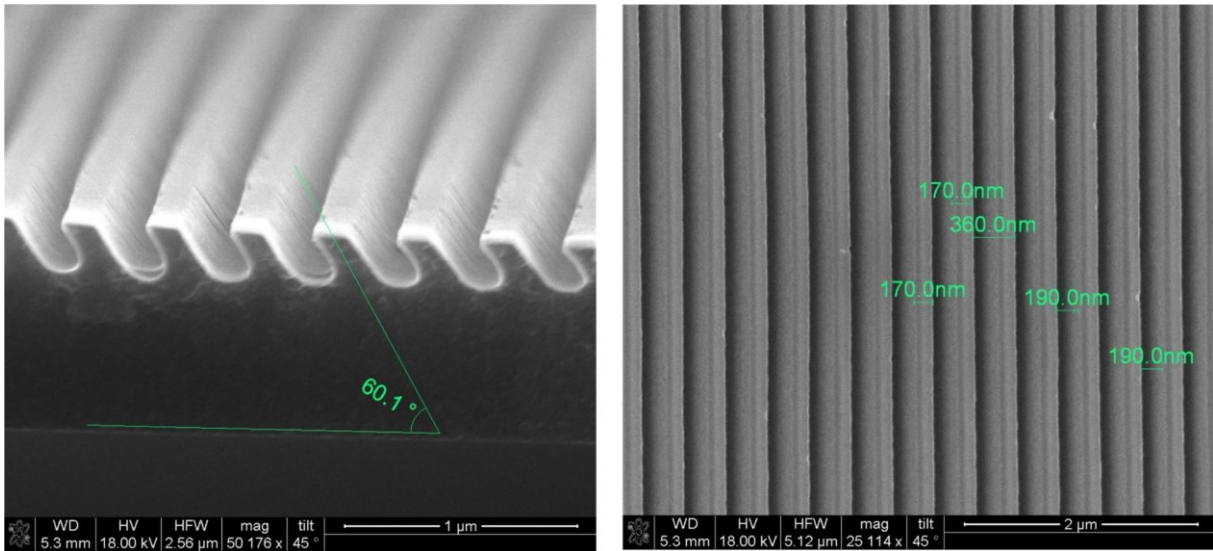
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Figure S1. Illustration of grating patterns on the waveguides (units, mm). Two pieces of waveguide are bonded with each other, and they were designed for a green-blue channel and a red channel, respectively. Three grating structures are nano-printed on the waveguide, and their relative locations are shown in the figure.



1
2 **Figure S2.** Illustration of diffraction structures nano-printed on waveguide surfaces (units, nm).
3 (a) and (b) provide the diffraction structures for the green-blue channel and red channel,
4 respectively.

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2 **Figure S3.** Top-view (left) and cross-sectional (right) SEM images of the in-coupling grating
3 for the green-blue channel waveguide.
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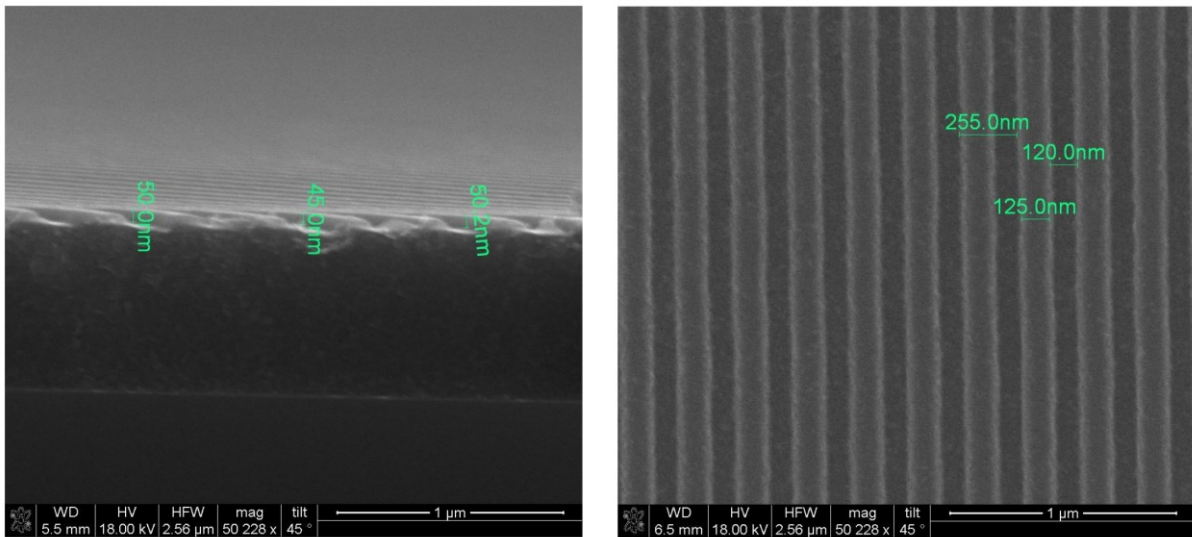
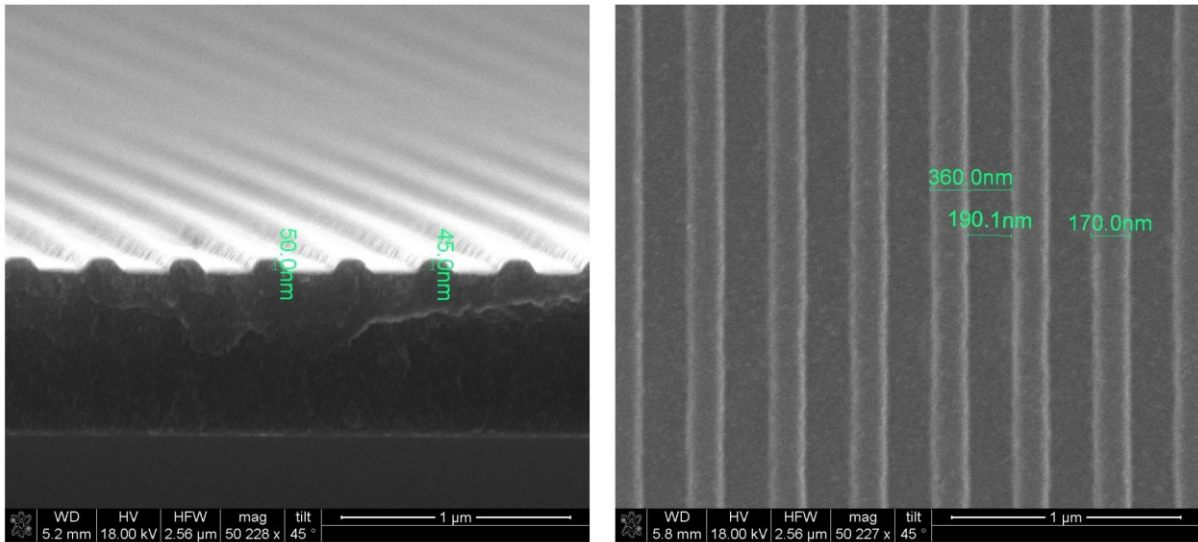
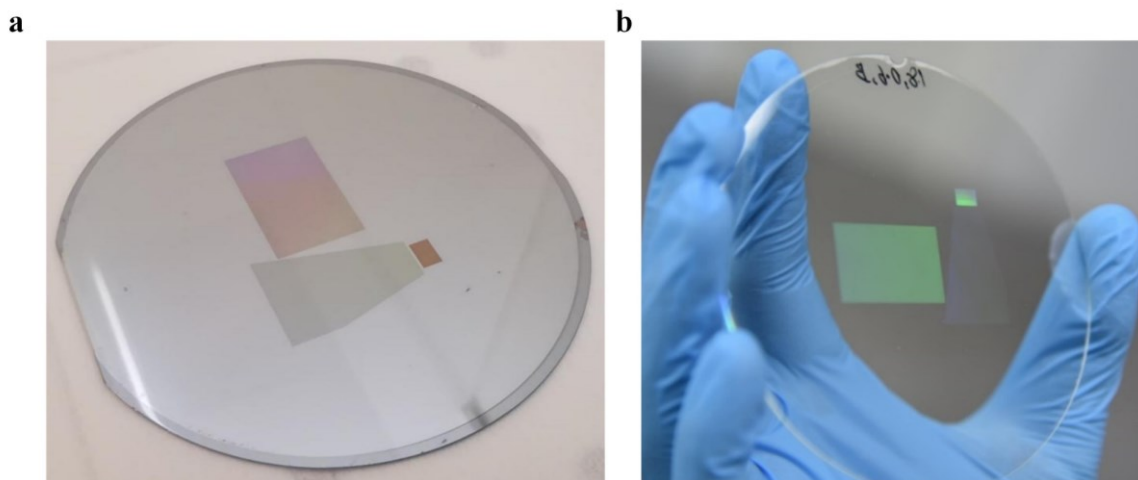


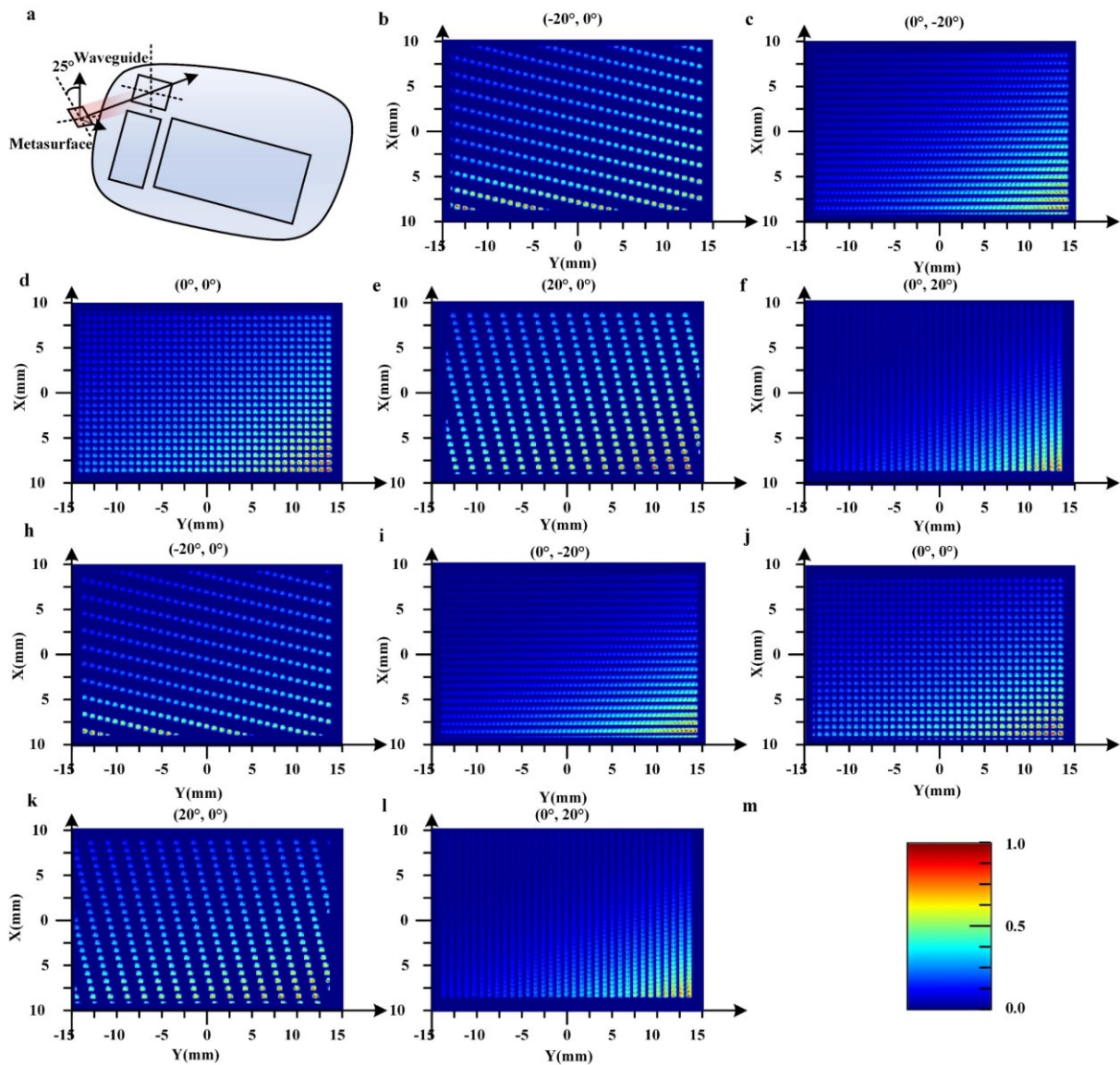
Figure S4. Cross-sectional (left) and top-view (right) SEM images of the turning grating for the green-blue channel waveguide.



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2 **Figure S5.** Cross-sectional (left) and top-view (right) SEM images of the outcoupling grating
3 for the green-blue channel waveguide.
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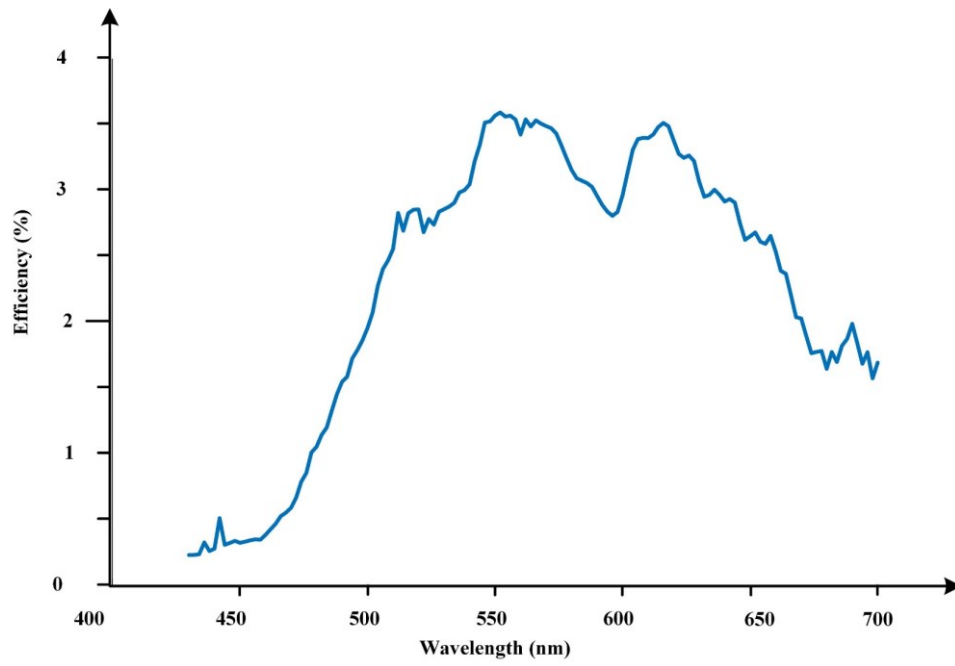


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2 **Figure S6.** Photographs of (a) imprint mold and (b) uncut waveguide, showing two steps of the
3 waveguide fabrication process.
4



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 2 **Figure S7.** Simulation results of beam distribution within the eye box for different fields of
 3 angles. The performance of the diffractive waveguide (with three gratings) and the metasurface
 4 ($0.5\text{mm} \times 0.5\text{mm}$) placed with a tilt of 25° to the waveguide normal are modeled in the
 5 simulation software. Five beams with different field of view ($(-20^\circ, 0^\circ)$, $(0^\circ, -20^\circ)$, $(0^\circ, 0^\circ)$, $(20^\circ,$
 6 $0^\circ)$, and $(0^\circ, -20^\circ)$) are irradiated from the metasurface and coupled to the input grating. A
 7 receiver is placed at the position of the viewer's eye, 15mm away from the output grating. Two
 8 types of waveguides are analyzed individually. (b-f) and (h-l) show the simulation results of the
 9 waveguide performance for the red channel and green-blue channel respectively. All the data
 10 in each image have been normalized and pseudo-colored (see (m) for the color scale). The
 11 distance between adjunct beams emitting from the waveguide should be less than 2mm within
 12 the overall eye box and the field of view.

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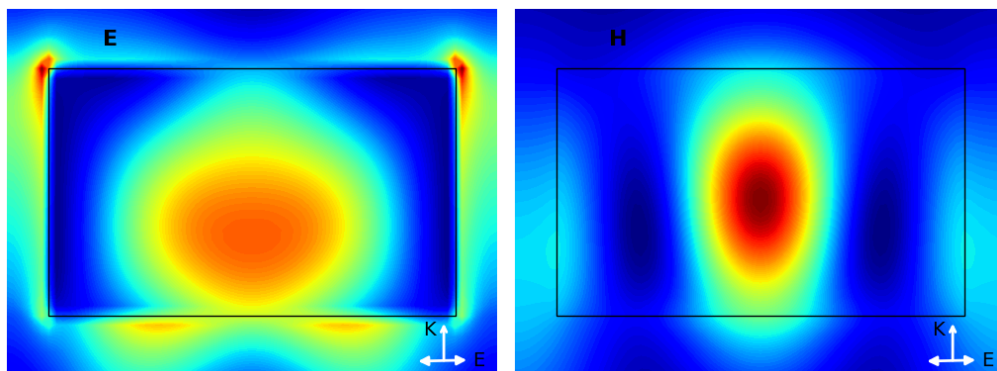


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2 **Figure S8.** Diffraction efficiency of the waveguide as a function of wavelength.

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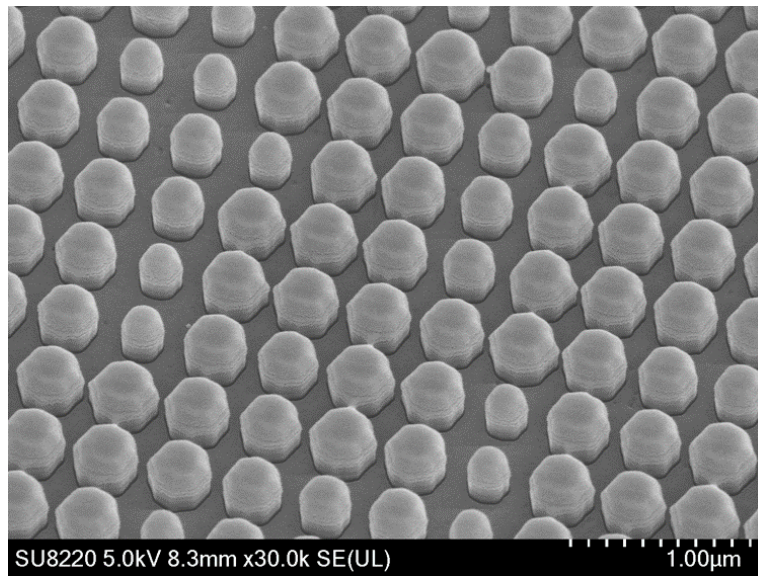
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3 **Figure S9.** The electric field profile (left) and magnetic field profile (right) in the nanodisk are
4 designed for the wavelength of 532nm at Huygens condition. The horizontal white arrow shows
5 the incident light polarisation and the vertical arrow indicates the light propagation direction.

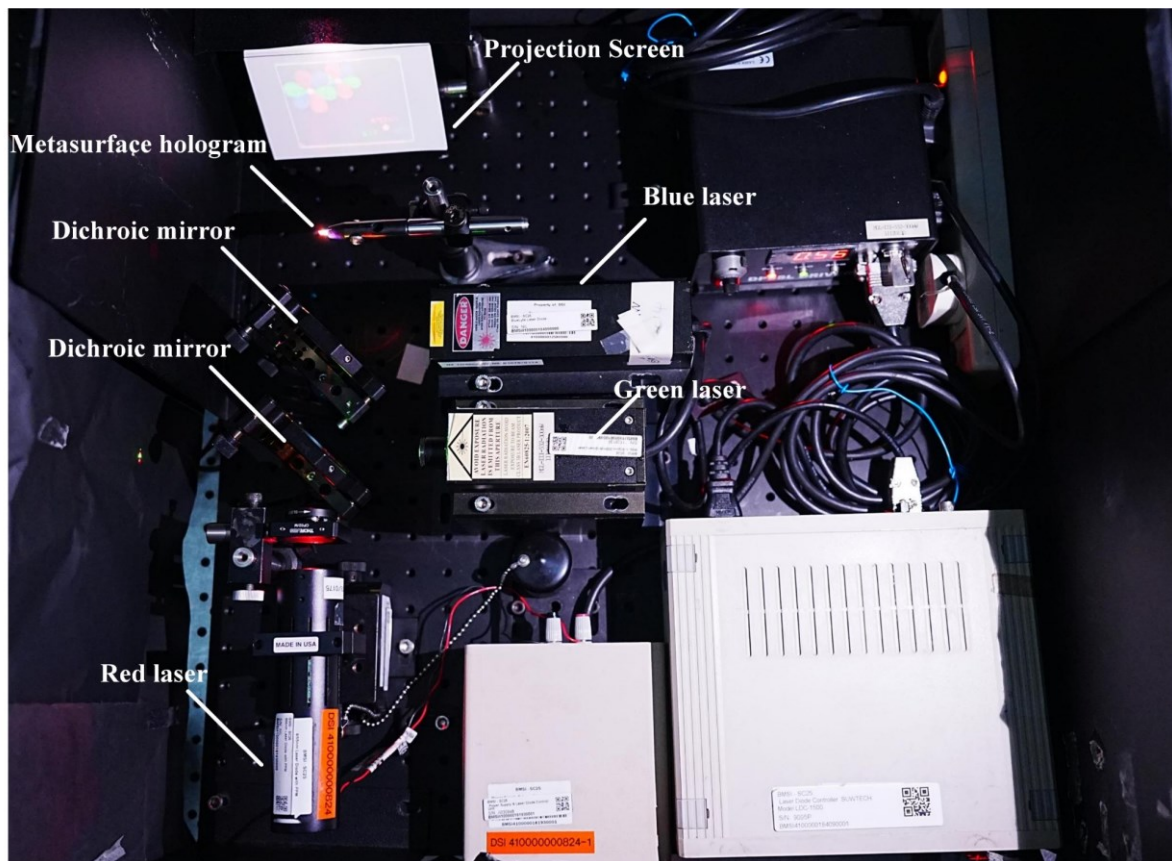
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3 **Figure S10.** SEM image of a metasurface hologram fabricated with the staircase fabrication
4 process.

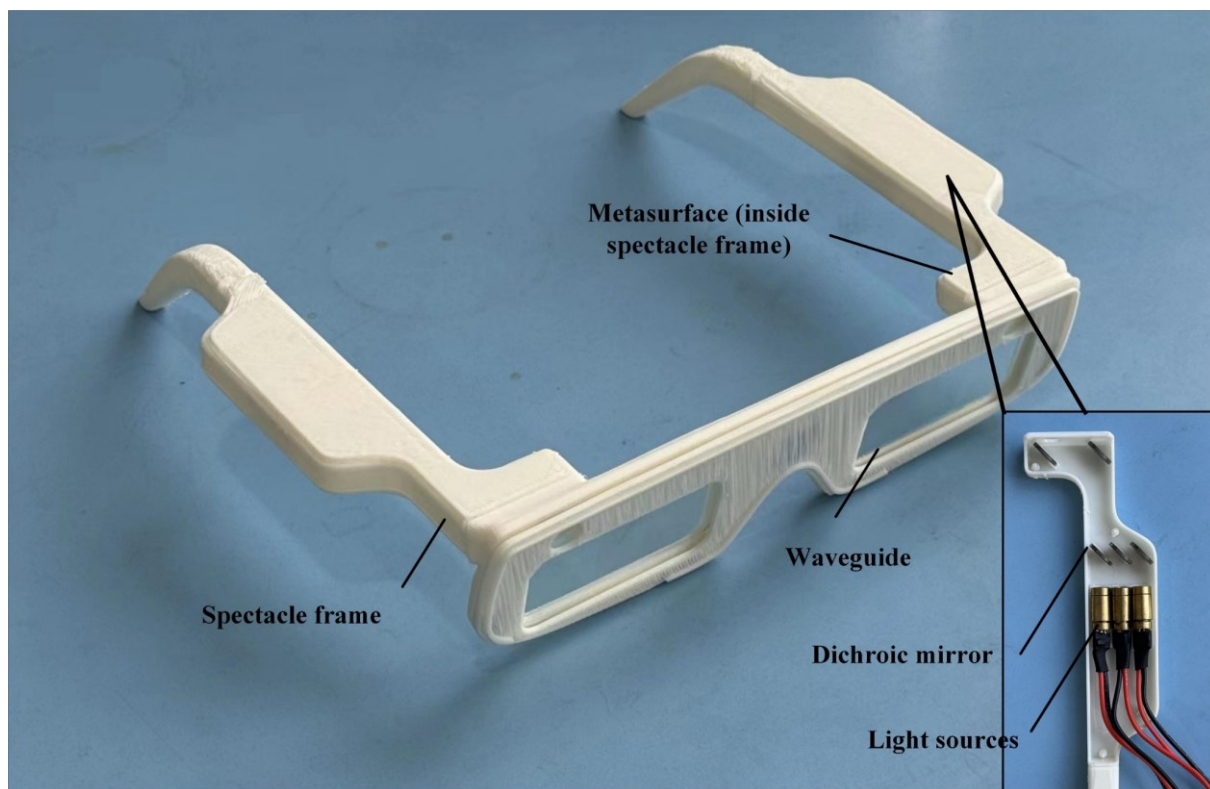
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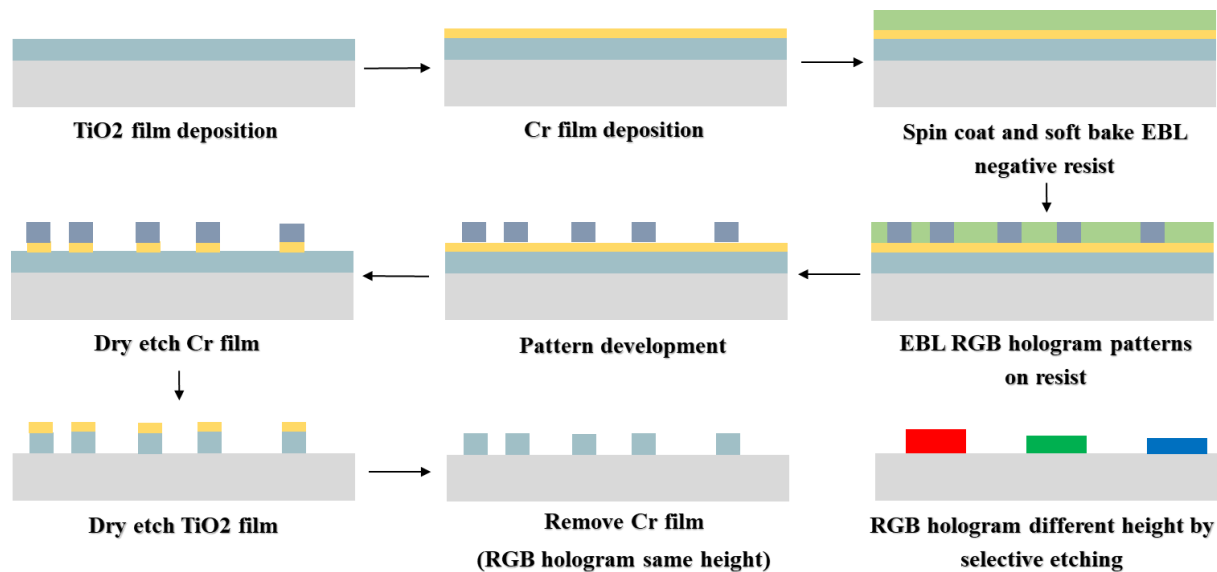
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2 **Figure S11.** System set-up for image projection using the designed metasurface holograms.

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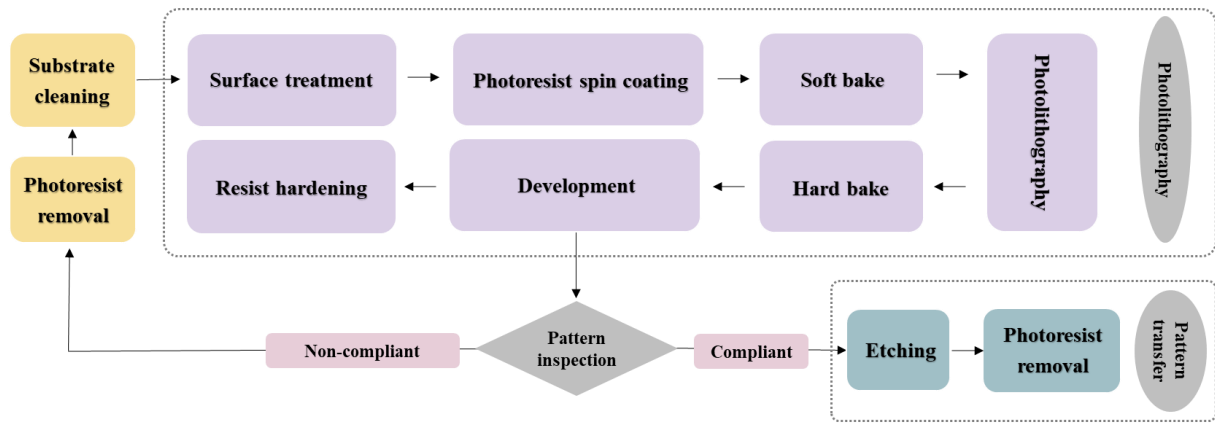


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2 **Figure S12.** Possible near-eye display system set-up using the designed metasurface holograms.
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Figure S13. Fabrication process of metasurface hologram.



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2 **Figure S14.** Fabrication process of nanoimprint mold.

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9 **Table S1** Design parameters of TiO₂-based transmissive Huygens' metasurfaces.

Wavelength (nm)	p (nm)	h (nm)	r (nm)
662 (Red)	420	172	185
532 (Green)	345	125	143
473 (Blue)	305	113	128

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Table S2 Simulated beam deflection efficiency at RGB wavelengths for the blazed gratings.

Wavelength (nm)	0 th diffraction order transmission	+1 st diffraction order transmission	-1 st diffraction order transmission	T (total transmission)
662 (Red)	16.5%	30.2%	0.37%	72.0%
532 (Green)	10.8%	36.0%	0.22%	72.3%
473 (Blue)	8.9%	32.5%	0.26%	73.4%

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